

<b>BCN</b>	<b>YD</b> 94	<b>TD</b> 95 / 98.7	<b>OW</b> 48 / 51.9	<b>IW</b> 16 / 18.1
	<b>EY</b> 31	/ 28.6	[A=(9+1) C=(6+1) K=(13+0) R=(1+0)]	
<b>BCN</b>	<b>YD</b> 76	<b>TD</b> 76 / 79.7	<b>OW</b> 35 / 41.8	<b>IW</b> 13 / 15.6
	<b>EY</b> 28	/ 22.3	[A=(9+1) C=(5+1) K=(11+0) R=(1+0)]	
<b>BCNAHSM1</b>	<b>YD</b> 5	<b>TD</b> 6 / 6.2	<b>OW</b> 3 / 3.6	<b>IW</b> 2 / 0.6
	<b>EY</b> 1	/ 2.0	[A=(0+0) C=(0+0) K=(1+0) R=(0+0)]	
<b>BCNHL</b>	<b>YD</b> 13	<b>TD</b> 13 / 12.8	<b>OW</b> 10 / 6.5	<b>IW</b> 1 / 1.9
	<b>EY</b> 2	/ 4.4	[A=(0+0) C=(1+0) K=(1+0) R=(0+0)]	
<b>MO</b> =[36](Ld-32 + Ey-4)		<b>TO</b> =[36](Ld-19/6 + Ey-17)		
		Dly / TTL / Avg EMPTY I.V FC	Dly / TTL / Avg EMPTY I.V FC	
<b>EC</b>	0/3/0.1		3/17/0.6	1/5/0.1
JNN	0/2/0.0			
RJB	0/1/0.0		2/14/0.5	1/5/0.1
TIS			0/2/0.0	
TORI			1/1/0.0	
<b>ECO</b>	<b>4/103/3.6</b>	2/33/1.1	<b>4</b>	<b>0/3/0.1</b>
NYG	0/12/0.4			1
RLJC	4/91/3.2	2/33/1.1	4	0/2/0.0
<b>ER</b>	<b>0/1/0.0</b>		<b>14/292/10.4</b>	<b>1/74/2.6</b>
ASN			1/16/0.5	1/9/0.3
BTNG	0/1/0.0		9/223/7.9	0/59/2.1
KPK			3/43/1.5	0/2/0.0
TPKR			1/10/0.3	0/4/0.1
<b>SEC</b>			<b>0/2/0.0</b>	
JSG			0/2/0.0	
<b>TOT</b>	<b>4/107/3.8</b>	2/33/1.1	<b>4</b>	<b>17/314/11.2</b>
			2/79/2.8	<b>8</b>
<b>FC:</b>	<b>MO</b> [31] (Ld-27 + Ey-4 )		<b>TO</b> [31] (Ld-23/5 + Ey-8 )	
<b>BOBRN</b>	<b>YD</b> 31	<b>TD</b> 30 / 25.9	<b>OW</b> 9 / 8.1	<b>IW</b> 16 / 8.3
	<b>EY</b> 5	/ 9.5	[A=(2+0) C=(3+0) K=(0+0) R=(0+0)]	
<b>MO</b> =[6](Ld-5 + Ey-1)		<b>TO</b> =[6](Ld-4/4 + Ey-2)		
		Dly / TTL / Avg EMPTY I.V FC	Dly / TTL / Avg EMPTY I.V FC	
<b>EC</b>	0/2/0.0			
JNN	0/1/0.0			
RJB	0/1/0.0			
<b>ECO</b>	<b>1/1/0.0</b>		<b>2/54/1.9</b>	<b>1</b>
JSG			2/54/1.9	1
RLJC	1/1/0.0			
<b>ER</b>	<b>0/29/1.0</b>		<b>1</b>	<b>0/4/0.1</b>
KPK	0/29/1.0		1	0/3/0.1
TPKR			0/1/0.0	0/2/0.0
<b>SEC</b>			<b>0/1/0.0</b>	
JSG			0/1/0.0	
<b>TOT</b>	<b>1/32/1.1</b>	<b>0/0/0.0</b>	<b>1</b>	<b>2/59/2.1</b>
			<b>0/2/0.0</b>	<b>1</b>
<b>FC:</b>	<b>MO</b> [8] (Ld-7 + Ey-1 )		<b>TO</b> [9] (Ld-8/8 + Ey-1 )	
<b>BOST</b>	<b>YD</b> 10	<b>TD</b> 11 / 19.5	<b>OW</b> 6 / 8.2	<b>IW</b> 2 / 1.7
	<b>EY</b> 3	/ 9.6	[A=(0+0) C=(1+1) K=(0+0) R=(1+0)]	
<b>MO</b> =[1](Ld-1 + Ey-0)		<b>TO</b> =[2](Ld-1/0 + Ey-1)		
		Dly / TTL / Avg EMPTY I.V FC	Dly / TTL / Avg EMPTY I.V FC	
<b>EC</b>	0/2/0.0		1/55/1.9	1
BRKA			0/7/0.2	1
JNN			0/3/0.1	
RJB			0/9/0.3	
TIS			0/15/0.5	
TORI	0/2/0.0		1/21/0.7	
<b>ECO</b>	<b>0/6/0.2</b>		<b>0/1/0.0</b>	
NYG	0/2/0.0			
RLJC	0/4/0.1		0/1/0.0	
<b>ER</b>			<b>0/5/0.1</b>	
ASN			0/1/0.0	
BTNG			0/3/0.1	
KPK			0/1/0.0	
<b>TOT</b>	<b>0/8/0.2</b>	<b>0/0/0.0</b>		<b>1/61/2.1</b>
			<b>0/0/0.0</b>	<b>1</b>
<b>FC:</b>	<b>MO</b> [2] (Ld-2 + Ey-0 )		<b>TO</b> [3] (Ld-2/0 + Ey-1 )	

<b>BOXN</b>	<b>YD</b> 527	<b>TD</b> 528 / 509.2	<b>OW</b> 155 / 155.0	<b>IW</b> 179 / 170.8
	<b>EY</b> 194	/ 183.4	[A=(38+2) C=(104+4) K=(41+0) R=(5+0)]	
<b>BOXN</b>	<b>YD</b> 162	<b>TD</b> 170 / 165.0	<b>OW</b> 62 / 61.6	<b>IW</b> 54 / 52.1
	<b>EY</b> 54	/ 51.3	[A=(11+2) C=(31+0) K=(8+0) R=(2+0)]	
<b>BOXNEL</b>	<b>YD</b> 3	<b>TD</b> 4 / 1.9	<b>OW</b> 1 / 0.8	<b>IW</b> 1 / 0.5
	<b>EY</b> 2	/ 0.6	[A=(0+0) C=(1+0) K=(0+0) R=(1+0)]	
<b>BOXNHL</b>	<b>YD</b> 337	<b>TD</b> 331 / 321.9	<b>OW</b> 85 / 85.7	<b>IW</b> 119 / 111.9
	<b>EY</b> 127	/ 124.4	[A=(27+0) C=(67+4) K=(27+0) R=(2+0)]	
<b>BOXNHL25</b>	<b>YD</b> 12	<b>TD</b> 9 / 10.7	<b>OW</b> 4 / 3.1	<b>IW</b> 2 / 3.8
	<b>EY</b> 3	/ 3.9	[A=(0+0) C=(1+0) K=(2+0) R=(0+0)]	
<b>BOXNS</b>	<b>YD</b> 13	<b>TD</b> 14 / 9.6	<b>OW</b> 3 / 3.9	<b>IW</b> 3 / 2.5
	<b>EY</b> 8	/ 3.3	[A=(0+0) C=(4+0) K=(4+0) R=(0+0)]	
<b>MO</b> =[92](Ld-78 + Ey-14)		<b>TO</b> =[92](Ld-80/49 + Ey-12)		
		Dly / TTL / Avg EMPTY I.V FC	Dly / TTL / Avg EMPTY I.V FC	
<b>EC</b>	0/5/0.1		1/38/1.3	0/3/0.1
BRKA	0/3/0.1		0/8/0.2	
GMO			0/1/0.0	0/1/0.0
PEH			0/3/0.1	
RJB	0/1/0.0		0/3/0.1	0/2/0.0
TIS			0/16/0.5	1
TORI	0/1/0.0		1/7/0.2	
<b>ECO</b>	<b>14/372/13.2</b>	0/29/1.0	<b>15</b>	<b>1/67/2.3</b>
JSG	0/2/0.0			0/3/0.1
NYG	2/44/1.5		3	1/38/1.3
RLJC	12/326/11.6	0/29/1.0	12	0/21/0.7
<b>ER</b>	<b>0/8/0.2</b>		<b>10/474/16.9</b>	<b>5/102/3.6</b>
ASN	0/2/0.0		1/68/2.4	1/27/0.9
BTNG	0/1/0.0		3/134/4.7	3/45/1.6
KPK	0/5/0.1		6/249/8.8	1/29/1.0
TPKR			0/23/0.8	2
<b>SEC</b>	<b>0/2/0.0</b>		<b>0/24/0.8</b>	<b>0/9/0.3</b>
JSG	0/2/0.0		0/24/0.8	0/9/0.3
<b>TOT</b>	<b>14/387/13.8</b>	0/29/1.0	<b>15</b>	<b>12/603/21.5</b>
			<b>5/117/4.1</b>	<b>23</b>
<b>FC:</b>	<b>MO</b> [111] (Ld-96 + Ey-15 )		<b>TO</b> [111] (Ld-88/60 + Ey-23 )	
<b>STEEL</b>	<b>YD</b> 85	<b>TD</b> 84 / 87.3	<b>OW</b> 25 / 23.8	<b>IW</b> 22 / 20.7
	<b>EY</b> 37	/ 42.8	[A=(6+2) C=(14+6) K=(4+0) R=(5+0)]	
<b>MO</b> =[14](Ld-14 + Ey-0)		<b>TO</b> =[11](Ld-5/2 + Ey-6)		
		Dly / TTL / Avg EMPTY I.V FC	Dly / TTL / Avg EMPTY I.V FC	
<b>EC</b>	0/11/0.3		4/183/6.5	2
BRKA	0/1/0.0		2/34/1.2	
GMO			0/2/0.0	
JNN	0/2/0.0		0/12/0.4	
RJB			0/37/1.3	2
TIS			1/30/1.0	
TORI	0/8/0.2		1/68/2.4	
<b>ECO</b>	<b>0/64/2.2</b>		<b>1</b>	<b>0/3/0.1</b>
JSG	0/7/0.2		1	
NYG	0/7/0.2			
RLJC	0/50/1.7		0/3/0.1	
<b>ER</b>	<b>0/1/0.0</b>		<b>2/68/2.4</b>	<b>1</b>
ASN	0/1/0.0		1/12/0.4	
BTNG			1/46/1.6	1
KPK			0/7/0.2	
TPKR			0/3/0.1	
<b>SEC</b>	<b>0/20/0.7</b>		<b>2</b>	<b>0/2/0.0</b>
JSG	0/20/0.7		2	0/2/0.0
<b>TOT</b>	<b>0/96/3.4</b>	<b>0/0/0.0</b>	<b>3</b>	<b>6/256/9.1</b>
			<b>0/0/0.0</b>	<b>3</b>
<b>FC:</b>	<b>MO</b> [12] (Ld-9 + Ey-3 )		<b>TO</b> [7] (Ld-4/0 + Ey-3 )	

<b>TOTL TRAIN</b>	<b>YD</b> 892	<b>TD</b> 892 / 882.8	<b>OW</b> 275 / 273.6	<b>IW</b> 296 / 281.0
	<b>EY</b> 321 / 328.3	[A=(60+6) C=(145+13) K=(80+0) R=(17+0)]		

<b>MO</b> =[177](Ld-148 + Ey-29)		<b>TO</b> =[174](Ld-128/67 + Ey-46)	
<b>Y-DayPerf</b> <b>Dly/TTL/Avg(Ly)</b>		<b>Y-DayPerf</b> <b>Dly/TTL/Avg(Ly)</b>	
<b>Ld</b>	<b>C</b>	<b>Ld</b>	<b>C</b>
EC	35/909/32.4(32.1)	29 + 1	31/796/28.4(31.6)
BRKA	9/249/8.8(10.1)	8 + 0	11/254/9.0(9.7)
GMO	3/113/4.0(4.7)	4 + 0	1/45/1.6(3.1)
JNN	2/39/1.3(1.3)	2 + 0	3/69/2.4(1.3)
PEH	3/57/2.0(2.1)	2 + 0	2/42/1.5(1.8)
RJB	12/221/7.8(10.0)	9 + 0	8/1967/0(10.8)
TIS	5/161/5.7(2.6)	3 + 1	2/78/2.7(2.0)
TORI	1/69/2.4(1.1)	1 + 0	4/112/4.0(2.6)
ECO	<b>61/1588/56.7(53.1)</b>	<b>36 + 24</b>	<b>60/1641/58.6(53.9)</b>
JSG	11/257/9.1(7.6)	11 + 1	11/252/9.0(7.6)
NYG	15/458/16.3(18.0)	13 + 3	18/473/16.8(16.3)
RLJC	35/873/31.1(27.5)	12 + 20	31/916/32.7(30.0)
ER	<b>57/1547/55.2(54.4)</b>	<b>70 + 1</b>	<b>52/1439/51.3(54.0)</b>
ASN	5/142/5.0(5.6)	10 + 0	5/138/4.9(4.9)
BTNG	29/729/26.0(22.4)	27 + 0	27/713/25.4(26.7)
KPK	22/582/20.7(22.7)	30 + 1	17/510/18.2(21.7)
TPKR	1/94/3.3(3.6)	3 + 0	3/78/2.7(0.5)
SEC	<b>24/655/23.3(26.6)</b>	<b>26 + 2</b>	<b>31/812/29.0(30.8)</b>
JSG	24/655/23.3(26.6)	26 + 2	31/812/29.0(30.8)
<b>TOT</b>	<b>177/4699/167.8(166.5)</b>	<b>161 + 28</b>	<b>174/4688/167.4(170.5)</b>
			<b>145/82 + 49</b>

<b>MO</b>	<b>YESTERDAY INTERCHANGE STOCKWISE</b>						
	<b>TO</b>	<b>BOXN</b>	<b>BCN</b>	<b>BOBRN</b>	<b>STEEL</b>	<b>OTHERS</b>	
EC	<b>20 + 0</b>	<b>4 + 0</b>	<b>1 + 0</b>	<b>6 + 0</b>	<b>4 + 0</b>	<b>35 + 0</b>	
	<b>13 + 1</b>	<b>3 + 3</b>	<b>0 + 0</b>	<b>2 + 5</b>	<b>0 + 4</b>	<b>18 + 13</b>	
BRKA	4 + 0	0 + 0	1 + 0	3 + 0	1 + 0	9 + 0	
	6 + 0	1 + 0	0 + 0	0 + 2	0 + 2	7 + 4	
GMO	2 + 0	0 + 0	0 + 0	0 + 0	1 + 0	3 + 0	
	0 + 0	1 + 0	0 + 0	0 + 0	0 + 0	1 + 0	
JNN	2 + 0	0 + 0	0 + 0	0 + 0	0 + 0	2 + 0	
	1 + 0	0 + 0	0 + 0	1 + 0	0 + 0	3 + 0	
PEH	3 + 0	0 + 0	0 + 0	0 + 0	0 + 0	3 + 0	
	2 + 0	0 + 0	0 + 0	0 + 0	0 + 0	2 + 0	
RJB	4 + 0	3 + 0	0 + 0	3 + 0	2 + 0	12 + 0	
	4 + 0	0 + 2	0 + 0	1 + 0	0 + 1	5 + 3	
TIS	5 + 0	0 + 0	0 + 0	0 + 0	0 + 0	5 + 0	
	0 + 0	0 + 0	0 + 0	0 + 1	0 + 1	0 + 2	
TORI	0 + 0	1 + 0	0 + 0	0 + 0	0 + 0	1 + 0	
	0 + 1	0 + 1	0 + 0	0 + 2	0 + 0	0 + 4	
ECO	<b>22 + 14</b>	<b>2 + 4</b>	<b>3 + 1</b>	<b>2 + 0</b>	<b>7 + 6</b>	<b>36 + 25</b>	
	<b>34 + 1</b>	<b>9 + 0</b>	<b>1 + 2</b>	<b>2 + 0</b>	<b>10 + 1</b>	<b>56 + 4</b>	
JSG	4 + 0	2 + 0	3 + 0	1 + 0	1 + 0	11 + 0	
	5 + 0	2 + 0	0 + 2	1 + 0	1 + 0	9 + 2	
NYG	12 + 2	0 + 0	0 + 0	0 + 0	0 + 1	12 + 3	
	11 + 1	0 + 0	0 + 0	1 + 0	5 + 0	17 + 1	
RLJC	6 + 12	0 + 4	0 + 1	1 + 0	6 + 5	13 + 22	
	18 + 0	7 + 0	1 + 0	0 + 0	4 + 1	30 + 1	
ER	<b>23 + 0</b>	<b>21 + 0</b>	<b>1 + 0</b>	<b>4 + 0</b>	<b>5 + 3</b>	<b>54 + 3</b>	
	<b>8 + 10</b>	<b>2 + 14</b>	<b>3 + 0</b>	<b>1 + 2</b>	<b>9 + 3</b>	<b>23 + 29</b>	
ASN	3 + 0	2 + 0	0 + 0	0 + 0	0 + 0	5 + 0	
	0 + 1	0 + 1	0 + 0	0 + 1	1 + 1	1 + 4	
BTNG	3 + 0	15 + 0	0 + 0	4 + 0	5 + 2	27 + 2	
	5 + 3	2 + 9	0 + 0	1 + 1	5 + 1	13 + 14	
KPK	17 + 0	3 + 0	1 + 0	0 + 0	0 + 1	21 + 1	
	3 + 6	0 + 3	3 + 0	0 + 0	2 + 0	8 + 9	
TPKR	0 + 0	1 + 0	0 + 0	0 + 0	0 + 0	1 + 0	
	0 + 0	0 + 1	0 + 0	0 + 0	1 + 1	1 + 2	
SEC	<b>13 + 0</b>	<b>5 + 0</b>	<b>0 + 0</b>	<b>3 + 0</b>	<b>2 + 1</b>	<b>23 + 1</b>	
	<b>25 + 0</b>	<b>5 + 0</b>	<b>0 + 0</b>	<b>1 + 0</b>	<b>0 + 0</b>	<b>31 + 0</b>	
JSG	13 + 0	5 + 0	0 + 0	3 + 0	2 + 1	23 + 1	
	25 + 0	5 + 0	0 + 0	1 + 0	0 + 0	31 + 0	
<b>TTL</b>	<b>78 + 14</b>	<b>32 + 4</b>	<b>5 + 1</b>	<b>15 + 0</b>	<b>18 + 10</b>	<b>148 + 29</b>	
	<b>80 + 12</b>	<b>19 + 17</b>	<b>4 + 2</b>	<b>6 + 7</b>	<b>19 + 8</b>	<b>128 + 46</b>	

<b>INTER DIVISIONAL SUMMARY</b>		<b>MADE OVER</b>	<b>TAKE OVER</b>
		<b>Dly/TTL/Avg(Ly)</b>	<b>Dly/TTL/Avg(Ly)</b>
<b>ADRA</b>	ADRA-CKP	CNI 39/989/35.3[38.0]	47/1096/39.1[42.9]
	ADRA-KGP	MDN 12/352/12.5[10.5]	17/426/15.2[13.1]
	ADRA-RNC	CNI 13/266/9.5[12.7]	12/266/9.5[9.6]
	ADRA-RNC	KSX 13/343/12.2[13.7]	14/352/12.5[13.4]
<b>CKP</b>	CKP-KGP	ASB 35/967/34.5[32.5]	29/912/32.5[33.2]
	CKP-RNC	NXN 17/501/17.8[13.3]	16/479/17.1[17.6]
	<b>TOTAL</b>	<b>129/3418/122.0[121.0]</b>	<b>135/3531/126.1[130.0]</b>

<b>DSLLOCO</b>	<b>TOTAL</b>	<b>ADRA</b>	<b>CKP</b>	<b>KGP</b>	<b>RNC</b>
HLDG/AVG	118/125	14/15	61/60	37/43	6/6
DU/AVG	107/109	13/13	51/50	37/39	6/5
OTG/AVG	122.6/162.4	16.0/21.5	61.9/79.0	40.3/52.2	4.5/9.6
WDG3	5/4	0/0	3/3	0/0	2/0
WDG4	113/120	14/15	58/56	37/42	4/5
EKM/AVG	427.2/384.5	356.9/354.4	431.6/423.2	461.7/358.4	308.1/276.4

  

<b>ELELOCO</b>	<b>TOTAL</b>	<b>ADRA</b>	<b>CKP</b>	<b>KGP</b>	<b>RNC</b>
HLDG/AVG	1065/1037	174/151	609/614	187/171	95/100
DU/AVG	715/703	112/98	399/406	140/130	64/68
OTG/AVG	1134.9/1111.2	173.8/154.4	614.0/598.0	265.1/259.1	82.0/99.6
G7 (MU)	101/92	18/16	54/52	12/13	17/10
G5 (MU)	6/8	1/1	2/3	2/2	1/0
G9 (MU)	264/261	47/39	171/175	25/22	21/24
G-12	19/15	5/2	9/7	5/4	0/1
EKM/AVG	303.5/301.3	321.4/308.4	310.4/307.9	251.2/268.0	383.1/336.7

<b>LOADING</b>	<b>TOTAL</b>	<b>ADRA</b>	<b>CKP</b>	<b>KGP</b>	<b>RNC</b>
LYR LDG	8574/8156.9	1286/1045.0	5945/5920.2	1168/1055.	175/136.1
	SE-(3754/3328.4)	SE-(222/2361.1)	SE-(748/683.8)	5	SE-(58/78.5)
LYR RK	159/151.6	23/19.5	108/108.7	24/20.9	3/2.4
	SE-(65/59.1)	SE-(3/3.4)	SE-(48/41.8)	SE-(13/12.4)	SE-(1/1.4)
CYR LDG	7368/7432.4	1034/863.9	5203/5341.6	1075/1112.	56/114.5
	SE-(3099/3107.0)	SE-(406/255.2)	SE-(2030/2105.5)	2	SE-(0/72.3)
CYR RK	139/139.0	19/16.3	97/98.5	22/22.0	1/2.0
	SE-(55/55.5)	SE-(7/4.2)	SE-(36/37.8)	SE-(12/12.2)	SE-(0/1.2)
N LDG(RK)	77/82.0	7/7.4	56/59.2	13/13.4	1/1.8
	SE-(26/29.6)	SE-(0/1.1)	SE-(15/16.3)	SE-(11/10.9)	SE-(0/1.2)
N-(HL)(RK)	24/32.3	0/2.1	23/28.9	1/1.0	0/0.2
	SE-(5/7.4)	SE-(0/0.7)	SE-(5/5.7)	SE-(0/0.8)	SE-(0/0.1)
N-25T(RK)	14/14.6	1/0.1	12/14.0	1/0.4	0/0.0
	SE-(5/6.3)	SE-(0/0.0)	SE-(4/5.8)	SE-(1/0.4)	SE-(0/0.0)
B LDG(RK)	14/13.6	2/2.3	7/7.7	5/3.5	0/0.0
	SE-(2/1.8)	SE-(0/0.0)	SE-(2/1.5)	SE-(2/0.2)	SE-(0/0.0)
B-(HL)(RK)	1/1.3	0/0.0	1/1.3	0/0.0	0/0.0
	SE-(0/0.1)	SE-(0/0.0)	SE-(0/0.1)	SE-(0/0.0)	SE-(0/0.0)
BS LDG(RK)	15/14.7	0/0.0	15/14.7	0/0.0	0/0.0
	SE-(15/14.7)	SE-(0/0.0)	SE-(15/14.7)	SE-(0/0.0)	SE-(0/0.0)
BSM LDG(RK)	3/2.3	1/0.7	2/1.4	0/0.1	0/0.0
	SE-(0/0.6)	SE-(0/0.0)	SE-(0/0.6)	SE-(0/0.0)	SE-(0/0.0)
BST LDG(RK)	4/4.0	1/1.2	3/2.5	0/0.2	0/0.0
	SE-(1/0.2)	SE-(1/0.0)	SE-(0/0.2)	SE-(0/0.0)	SE-(0/0.0)
R LDG(RK)	10/6.9	5/2.7	5/4.1	0/0.0	0/0.0
	SE-(6/3.6)	SE-(5/2.5)	SE-(1/1.0)	SE-(0/0.0)	SE-(0/0.0)
ST LDG(RK)	9/7.2	3/1.6	6/5.3	0/0.1	0/0.0
	SE-(1/0.9)	SE-(1/0.3)	SE-(0/0.3)	SE-(0/0.1)	SE-(0/0.0)
Y LDG(RK)	3/2.2	0/0.0	3/2.2	0/0.0	0/0.0
	SE-(3/2.2)	SE-(0/0.0)	SE-(3/2.2)	SE-(0/0.0)	SE-(0/0.0)
N LDG(WG)	4317/4693.6	412/438.6	3125/3388.1	724/757.6	56/109.1
	SE-(1472/1697.1)	SE-(0/68.8)	SE-(857/939.8)	SE-(615/617.9)	SE-(0/70.4)</

## DIVISION WISE INWARD RELEASE UTILIZATION

	<b>IW</b>	<b>RL</b>	<b>UTIL</b>
<b>ADRA</b>	85/76.6	31/31.3	36.4/40.8
BCN	5/5.3	2/1.7	40.0/31.7
BOBRN	5/4.4	3/4.6	60.0/104.8
BOSM	0/0.1	0/0.0	0.0/33.3
BOST	1/0.2	0/0.0	0.0/25.0
BOXN	71/63.9	24/24.5	33.8/38.3
STEEL	3/2.4	2/0.3	66.6/14.7
<b>CKP</b>	<b>IW</b>	<b>RL</b>	<b>UTIL</b>
BCN	2/2.4	1/0.6	50.0/26.0
BOSM	1/1.6	0/0.5	0.0/34.7
BOST	0/0.3	0/0.1	0.0/50.0
BOXN	74/66.0	32/28.3	43.2/42.9
STEEL	9/7.8	0/0.7	0.0/10.0
<b>KGP</b>	<b>IW</b>	<b>RL</b>	<b>UTIL</b>
BCN	3/7.2	1/2.5	33.3/35.6
BOBRN	4/3.4	0/1.0	0.0/30.9
BOSM	2/1.3	1/0.4	50.0/32.4
BOST	0/1.1	0/0.5	0.0/50.0
BOXN	38/39.4	22/20.7	57.8/52.6
STEEL	6/6.2	2/1.2	33.3/19.3
<b>RNC</b>	<b>IW</b>	<b>RL</b>	<b>UTIL</b>
BCN	2/3.2	0/0.7	0.0/24.4
BOXN	0/1.2	0/1.1	0.0/91.6
STEEL	5/3.8	1/0.1	20.0/2.7

YDay Wgn	TOTL	ADRA	CKP	KGP	RNC
Hldg/Avg	50693/49704	10447/9194	25334/24997	12470/12314	2442/3198

## YESTERDAY UTILIZATION OF MAJOR STOCKS

	EY	LD	MO	Ut%	IW	RL	Ut%	OW	MO-F	Ut%
BCN	26/29.0	14/13.6	4/3.8	69.6/60.2	12/18.2	4/5.7	33.3/31.2	56/51.9	32/24.6	57.1/47.3
BOBRN	12/9.7	10/6.9	1/1.1	91.6/83.0	9/7.8	3/5.7	33.3/72.4	10/8.1	5/4.8	50.0/58.9
BOSM	7/11.7	3/2.3	1/0.9	57.1/27.8	3/3.0	1/1.0	33.3/33.7	7/5.5	5/2.5	71.4/46.1
BOST	5/9.8	4/4.0	0/0.2	80.0/43.6	1/1.7	0/0.8	0.0/46.0	4/8.2	1/3.5	25.0/43.2
BOXN	193/182.8	77/82.0	14/13.8	47.1/52.4	83/170.7	78/74.7	42.6/43.8	151/155.1	78/82.4	51.6/53.1
STEEL	36/42.6	9/7.2	0/3.4	25.0/25.0	23/20.4	5/2.4	21.7/12.0	26/23.8	14/9.7	53.8/40.6

I/C	WAG-5		WAG-7		WAG-9		G7 + G9		WAG-12	
	M/O	T/O	M/O	T/O	M/O	T/O	M/O	T/O	M/O	T/O
EC	0/0.7	0/0.6	3/4.3	4/3.3	19/13.7	7/9.3	22/18.1	11/12.6	3/2.6	2/2.5
ECO	2/1.1	2/1.4	7/8.1	9/7.6	20/19.6	26/19.1	27/27.7	35/26.7	1/1.7	0/2.2
ER	0/0.6	0/1.0	5/8.1	8/7.7	18/17.6	10/16.9	23/25.7	18/24.7	2/1.2	4/1.4
SEC	1/0.5	0/0.3	6/4.7	3/5.4	14/13.4	17/17.1	20/18.2	20/22.6	0/0.9	0/0.2
Total	3/3.1	2/3.3	21/25.2	24/24.2	71/64.5	60/62.5	92/89.8	84/86.7	6/6.6	6/6.5